AMENDMENTS TO THE SPECIFICATION

Please amend paragraph [0057] of the specification as follows:

Illustrated in FIG. 9 is a "B Section test tool" 100 (also known as the intermediate head test tool) which is secured inside the stack for use in pressure-integrity testing as described above with reference to FIG. 5. As explained, bull-nosed bottom portion 101 which has an annular shoulder for supporting above it a metal gauge ring 102, an elastomeric backup seal 103 and an elastomeric cup 104, which is preferably made of nitrile rubber, although other elastomers or polymers may be used. The cup 104 includes a pair of annular grooves 104a into which O-rings may be seated to provide a fluid-tight seal between the cup 104 and the bull-nosed bottom portion 101. The test plug 100 further includes a tubular extension 105 which is threaded at a bottom end to support the bull-nosed end portion 101. A top end of the tubular extension 105 is integrally formed with an upper shoulder 106. The upper shoulder 106 abuts an annular constriction in the drilling flange 40 as shown. When the upper shoulder 106 has abutted the annular constriction, the locking pins 46 in the drilling flange 40 are screwed inwardly to engage an upper surface of the upper shoulder 106, thereby securing the test plug inside the stack. The upper shoulder 106 further includes a plurality of fluid passages 107 through which fluid may flow during pressurization of the stack.

Please amend paragraph [0058] of the specification as follows:

The B section test plug 100 is inserted and retracted using the test plug landing tool 59, which is threaded to the test plug 100 inside an internally threaded socket 108, which extends upwardly from the upper shoulder 106, as described above. After the test plug landing tool 109 has been removed, the stack is

pressurized to at least an estimated operating pressure. Due to the design of the B section test plug 100, the pressure-integrity of the joint between the intermediate casing and the intermediate casing mandrel (as well as the pressure-integrity of all the joints and seals above it in the stack) are pressure tested.

Please amend paragraph [0073] of the specification as follows:

In some cases, the intermediate casing string 70 cannot be run to the desired depth because of debris or some other blockage at or near the bottom of the well bore, or because the string length was miscalculated. In that case, slips 170 are affixed to the intermediate casing 70, as illustrated in FIG. 15. The slips 170 are frusta-conically shaped to be seated in an upwardly flared casing bowl 38' of a wellhead 36'. As shown, the wellhead 36' is a variant of the wellhead 36. The wellhead 36' has a modified casing bowl 38', *i.e.*, the casing bowl 38' provides more angle with respect to the vertical and has a longer contact surface than the standard casing bowl 38. The casing bowl 38' is thus designed to support a tubular string using the slips 170. The casing bowl 38' includes side ports 37'.

Please amend paragraph [0084] of the specification as follows:

The flow-control stack 200 is flanged to a top flange 185 of the tubing head spool 180. The top flange 185 includes a ring gasket groove 186 which aligns with an annular groove 202 in the flow control stack 200 for receiving a standard metal ring gasket. The flow-control stack 200 may include any one or more of a flow tee, choke, master valve or production valves. These flow-control devices are well known in the art and are not described in further detail. The tubing hanger 182 also has a pair of annular grooves 183 in which O-rings are seated for providing a fluid-tight seal between the tubing head spool 180 and the tubing hanger 182.